JUSTIFICATION OF PROXY SU(3) THROUGH A NILSSON CALCULATION

- SU(3) is the symmetry group of the harmonic oscillator –present in the sd shell of a nucleus
- The symmetry of the harmonic oscillator is destroyed at higher major shells, mostly due to spin –orbit interaction
- The proxy SU(3) is a new symmetry scheme valid for deformed nuclei ,based on SU(3), which is established by replacing the "intruder" parity orbitals with their 0[110] partners
- The new shells that will emerge will have SU(3) symmetry, but how will be known that the approximation is valid?
- A mathematical justification through a Nilsson calculation is necessary

The Nilsson Hamiltonian for large deformations

$$H = H_{osc} + u_{ls}\hbar(l \cdot s) + u_{ll}\hbar\omega_0(l^2 - \langle l^2 \rangle_{\rm N})$$

-The eigenvalues of the terms H_{osc} and $\langle l^2 \rangle_N$ can be calculated directly because they are functions of N and n_z

-The eigenvalues of the terms $l \cdot s$ and l^2 must be calculated in the new basis

-The u_{ls} and u_{ll} are known parameters

| region | v_{ls} | v_{ll} | κ | μ |
|--------------|----------|----------|----------|-------|
| N, Z < 50 | -0.16 | 0 | 0.08 | 0 |
| 50 < Z < 82 | -0.127 | -0.0382 | 0.0635 | 0.602 |
| 82 < N < 126 | -0.127 | -0.0268 | 0.0635 | 0.422 |
| 82 < Z < 126 | -0.115 | -0.0375 | 0.0575 | 0.652 |
| 126 < N | -0.127 | -0.0206 | 0.0635 | 0.324 |

A. Bohr and B. R. Mottelson, Nuclear Structure, Vol. II: Nuclear Deformations (Benjamin, New York, 1975).

MATRIX ELEMENTS OF THE SPIN ORBIT TERM $l \cdot s$

- Diagonal matrix elements $\langle n_z rs\Sigma | l \cdot s | n_z rs\Sigma \rangle = (r-s)\Sigma = \Lambda\Sigma$
- Non diagonal matrix elements $\langle n_z 1, r, s, \Sigma 1 | l \cdot s | n_z r s \Sigma \rangle = -\frac{1}{\sqrt{2}} \sqrt{n_z (r+1)}$

$$\langle n_z + 1, r, s - 1, \Sigma - 1 | l \cdot s | n_z r s \Sigma \rangle = -\frac{1}{\sqrt{2}} \sqrt{(n_z + 1)s}$$

 $\langle n_z rs\Sigma | l \cdot s | n_z rs\Sigma \rangle = (r-s)\Sigma = \Lambda\Sigma$

$$\langle n_z rs\Sigma | l \cdot s | n_z rs\Sigma \rangle = (r-s)\Sigma = \Lambda\Sigma$$

Shapes and Shells in Nuclear Structure, by Ingemar Ragnarsson, Sven Gvsta Nilsson, Cambridge, UK: Cambridge University Press, 2005

MATRIX ELEMENTS OF THE SQUARE OF THE ANGULAR MOMENTUM l^2

• Diagonal matrix elements

$$\langle n_z r s \Sigma | l^2 | n_z r s \Sigma \rangle = 2n_z + (r + s + 1) + (r + s) + (r - s)^2$$

• Non diagonal matrix elements

$$\langle n_z + 2, r - 1, s, \Sigma | l^2 | n_z r s \Sigma \rangle = -2\sqrt{(n_z + 2)(n_z + 1)rs}$$

$$\langle n_z rs\Sigma | l^2 | n_z rs\Sigma \rangle = -2\sqrt{(n_z-1)n_z (r+1)(s+1)}$$

Shapes and Shells in Nuclear Structure, by Ingemar Ragnarsson, Sven Gvsta Nilsson, Cambridge, UK: Cambridge University Press, 2005

Matrix of $l \cdot s$ for the 50-82 shell

| | $\frac{1}{2}[400]$ | $\frac{1}{2}[411]$ | $\frac{3}{2}[402]$ | $\frac{1}{2}[420]$ | $\frac{3}{2}[411]$ | $\frac{5}{2}[402]$ | $\frac{1}{2}[431]$ | $\frac{3}{2}[422]$ | $\frac{5}{2}[413]$ | $\frac{7}{2}[404]$ | $\frac{1}{2}[550]$ | $\frac{3}{2}[541] \frac{5}{2}$ | [532] | $\frac{7}{2}[523] \frac{9}{2}$ | $[514] \frac{1}{2}$ | $\frac{1}{505}$ |
|-----------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------------------|-------|--------------------------------|---------------------|-----------------|
| 1/2[400] | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[411] | | -0.5 | 0 | -1.414 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3/2[402] | | | -1 | 0 | -1.225 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[420] | | | | 0 | 0 | 0 | 1.225 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3/2[411] | | | | | 0.5 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5/2[402] | | | | | | 1 | 0 | 0 | 0.707 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[431] | | | | | | | -0.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3/2[422] | | | | | | | | $^{-1}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5/2[413] | | | | | | | | | -1.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7/2[404] | | | | | | | | | | -2 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[550] | | | | | | | | | | | 0 | 0 | 0 | 0 | 0 | 0 |
| 3/2[541] | | | | | | | | | | | | 0.5 | 0 | 0 | 0 | 0 |
| 5/2[532] | | | | | | | | | | | | | 1 | 0 | 0 | 0 |
| 7/2[523] | | | | | | | | | | | | | | 1.5 | 0 | 0 |
| 9/2[514] | | | | | | | | | | | | | | | 2 | 0 |
| 11/2[505] | | | | | | | | | | | 2 | | | | | 2.5 |

Matrix of $l \cdot s$ for the sdg shell

| | $\frac{1}{2}[400]$ | $\frac{1}{2}[411]$ | $\frac{3}{2}[402]$ | $\frac{1}{2}[420]$ | $\frac{3}{2}[411]$ | $\frac{5}{2}[402]$ | $\frac{1}{2}[431]$ | $\frac{3}{2}[422]$ | $\frac{5}{2}[413]$ | $\frac{7}{2}[404]$ | $\frac{1}{2}[440]$ | $\frac{3}{2}[431]$ | $\frac{5}{2}[422]$ | $\frac{7}{2}[413]$ | $\frac{9}{2}[404]$ |
|----------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|
| 1/2[400] | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[411] | | -0.5 | 0 | -1.414 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3/2[402] | | | -1 | 0 | -1.225 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[420] | | | | 0 | 0 | 0 | 1.225 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3/2[411] | | | | | 0.5 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5/2[402] | | | | | | 1 | 0 | 0 | 0.707 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[431] | | | | | | | -0.5 | 0 | 0 | 0 | -1.414 | 0 | 0 | 0 | 0 |
| 3/2[422] | | | | | | | | $^{-1}$ | 0 | 0 | 0 | -1.732 | 0 | 0 | 0 |
| 5/2[413] | | | | | | | | | -1.5 | 0 | 0 | 0 | -1.732 | 0 | 0 |
| 7/2[404] | | | | | | | | | | $^{-2}$ | 0 | 0 | 0 | -1.414 | 0 |
| 1/2[440] | | | | | | | | | | | 0 | 0 | 0 | 0 | 0 |
| 3/2[431] | | | | | | | | | | | | 0.5 | 0 | 0 | 0 |
| 5/2[422] | | | | | | | | | | | | | 1 | 0 | 0 |
| 7/2[413] | | | | | | | | | | | | | | 1.5 | 0 |
| 9/2[404] | | | | | | | | | | | | | | | 2 |

Matrix of l^2 for the 50-82 shell

| | $\frac{1}{2}[400]$ | $\frac{1}{2}[411] \frac{3}{2}$ | $\frac{3}{5}[402]$ | $\frac{1}{2}[420]$ | $\frac{3}{2}[411] \frac{5}{2}$ | [402] | $\frac{1}{2}[431]$ | $\frac{3}{2}[422] \frac{5}{2}$ | $[413] \frac{7}{2}$ | $[404] \frac{1}{2}$ | $\frac{3}{5}[550]\frac{3}{2}$ | $[541] \frac{5}{2}$ | $[532]\frac{7}{2}$ | $[523] \frac{9}{2}$ | $[514] \frac{11}{2}$ | [505] |
|-----------|--------------------|--------------------------------|--------------------|--------------------|--------------------------------|-------|--------------------|--------------------------------|---------------------|-----------------------|-------------------------------|---------------------|--------------------|---------------------|----------------------|-------|
| 1/2[400] | 4 | 0 | 0 | -5.657 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[411] | | 12 | 0 | 0 | 0 | 0 | -6.928 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3/2[402] | | | 8 | 0 | 0 | 0 | 0 | -4.899 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[420] | | | | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3/2[411] | | | | | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5/2[402] | | | | | | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[431] | | | | | | | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3/2[422] | | | | | | | | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5/2[413] | | | | | | | | | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7/2[404] | | | | | | | | | | 20 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[550] | | | | | | | | | | | 10 | 0 | 0 | 0 | 0 | 0 |
| 3/2[541] | | | | | | | | | | | | 18 | 0 | 0 | 0 | 0 |
| 5/2[532] | | | | | | | | | | | | | 24 | 0 | 0 | 0 |
| 7/2[523] | | | | | | | | | | | | | | 28 | 0 | 0 |
| 9/2[514] | | | | | | | | | | | | | | | 30 | 0 |
| 11/2[505] | | | | | | | | | | 15 | | | | | | 30 |

Matrix of l^2 of sdg shell

| | $\frac{1}{2}[400]$ | $\frac{1}{2}[411]$ | $\frac{3}{2}[402]$ | $\frac{1}{2}[420]$ | $\frac{3}{2}[411]$ | [402] | $\frac{1}{2}[431]$ | $\frac{3}{2}[422]$ | $\frac{5}{2}[413]$ | $\frac{7}{2}[404]$ | $\frac{1}{2}[440]$ | $\frac{3}{2}[431]$ | $\frac{5}{2}[422]\frac{7}{2}$ | $[413] \frac{9}{2}$ | [404] |
|----------|--------------------|--------------------|--------------------|--------------------|--------------------|-------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|-------------------------------|---------------------|-------|
| 1/2[400] | 4 | 0 | 0 | -5.657 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[411] | | 12 | 0 | 0 | 0 | 0 | -6.928 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3/2[402] | | | 8 | 0 | 0 | 0 | 0 | -4.899 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[420] | | | | 14 | 0 | 0 | 0 | 0 | 0 | 0 | -6.928 | 0 | 0 | 0 | 0 |
| 3/2[411] | | | | | 12 | 0 | 0 | 0 | 0 | 0 | 0 | -6.928 | 0 | 0 | 0 |
| 5/2[402] | | | | | | 8 | 0 | 0 | 0 | 0 | 0 | 0 | -4.899 | 0 | 0 |
| 1/2[431] | | | | | | | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3/2[422] | | | | | | | | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5/2[413] | | | | | | | | | 20 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7/2[404] | | | | | | | | | | 20 | 0 | 0 | 0 | 0 | 0 |
| 1/2[440] | | | | | | | | | | ~ | 8 | 0 | 0 | 0 | 0 |
| 3/2[431] | | | | | | | | | | | | 14 | 0 | 0 | 0 |
| 5/2[422] | | | | | | | | | | | | | 18 | 0 | 0 |
| 7/2[413] | | | | | | | | | | | | | | 20 | 0 |
| 9/2[404] | | | | | | | | | | | | | | | 20 |

Matrix of the Hamiltonian for the 50-82 proton shell

| | $\frac{1}{2}[400]$ | $\frac{1}{2}[411]$ | $\frac{3}{2}[402]$ | $\frac{1}{2}[420]$ | $\frac{3}{2}[411]$ | $\frac{5}{2}[402]$ | $\frac{1}{2}[431]$ | $\frac{3}{2}[422]$ | $\frac{5}{2}[413]$ | $\frac{7}{2}[404]$ | $\frac{1}{2}[550]$ | $\frac{3}{2}[541]$ | $\frac{5}{2}[532]$ | $\frac{7}{2}[523]$ | $\frac{9}{2}[514]$ | $\frac{11}{2}[505]$ |
|-----------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|---------------------|
| 1/2[400] | 6.28 | -0.13 | 0 | 0.22 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[411] | | 5.74 | 0 | 0.18 | 0 | 0 | 0.27 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3/2[402] | | | 6.26 | 0 | 0.16 | 0 | 0 | 0.19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[420] | | | | 5.30 | 0 | 0 | -0.16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3/2[411] | | | | | 5.61 | 0 | 0 | -0.13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5/2[402] | | | | | | 6.00 | 0 | 0 | -0.09 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[431] | | | | | | | 5.06 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3/2[422] | | | | | | | | 5.27 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5/2[413] | | | | | | | | | 5.56 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7/2[404] | | | | | | | | | | 5.93 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2 550 | | | | | | | | | | | 5.88 | 0 | 0 | 0 | 0 | 0 |
| 3/2[541] | | | | | | | | | | | | 5.81 | 0 | 0 | 0 | 0 |
| 5/2[532] | | | | | | | | | | | | | 5.82 | 0 | 0 | 0 |
| 7/2[523] | | | | | | | | | | | | | | 5,90 | 0 | 0 |
| 9/2[514] | | | | | | | | | | | | | | | 6.06 | 0 |
| 11/2[505] | | | | | | | | | | | × | | | | | 6.30 |

Matrix of the Hamiltonian for the sdg proton shell

| | $\frac{1}{2}[400]$ | $\frac{1}{2}[411]$ | $\frac{3}{2}[402]$ | $\frac{1}{2}[420]$ | $\frac{3}{2}[411]$ | $\frac{5}{2}[402]$ | $\frac{1}{2}[431]$ | $\frac{3}{2}[422]$ | $\frac{5}{2}[413]$ | $\frac{7}{2}[404]$ | $\frac{1}{2}[440]$ | $\frac{3}{2}[431]$ | $\frac{5}{2}[422]$ | $\frac{7}{2}[413]$ | $\frac{9}{2}[404]$ |
|----------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|
| 1/2[400] | 6.28 | -0.13 | 0 | 0.22 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[411] | | 5.74 | 0 | 0.18 | 0 | 0 | 0.27 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3/2[402] | | | 6.26 | 0 | 0.16 | 0 | 0 | 0.19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[420] | | | | 5.30 | 0 | 0 | -0.16 | 0 | 0 | 0 | 0.27 | 0 | 0 | 0 | 0 |
| 3/2[411] | | | | | 5.61 | 0 | 0 | -0.13 | 0 | 0 | 0 | 0.27 | 0 | 0 | 0 |
| 5/2[402] | | | | | | 6.00 | 0 | 0 | -0.09 | 0 | 0 | 0 | 0.19 | 0 | 0 |
| 1/2[431] | | | | | | | 5.06 | 0 | 0 | 0 | 0.18 | 0 | 0 | 0 | 0 |
| 3/2[422] | | | | | | | | 5.27 | 0 | 0 | 0 | 0.22 | 0 | 0 | 0 |
| 5/2[413] | | | | | | | | | 5.56 | 0 | 0 | 0 | 0.22 | 0 | 0 |
| 7/2[404] | | | | | | | | | | 5.93 | 0 | 0 | 0 | 0.18 | 0 |
| 1/2[440] | | | | | | | | | | | 5.73 | 0 | 0 | 0 | 0 |
| 3/2[431] | | | | | | | | | | | | 5.74 | 0 | 0 | 0 |
| 5/2[422] | | | | | | | | | | | | | 5.82 | 0 | 0 |
| 7/2[413] | | | | | | | | | | | | | | 5.98 | 0 |
| 9/2[404] | | | | | | | | | | | | | | | 6.22 |

• The matrices are symmetric so only the diagonal and the upper part is shown.

 A very small percentage is affected by the approximations in the proxy SU(3) scheme!!

• The SU(3) symmetry is conserved!!





- As we move to heavier shells the approximation gets better!
- In the sdg shell 8.44% of the matrix elements are affected by the approximations, in the pfh shell the number drops to 5.44% and in the sdgi shell at 3.70%

| shell | $l \cdot s$ | l^2 | H | total |
|-------|-------------|-----------------|----|-------|
| pf | 6 | . . | 6 | 100 |
| sdg | 8 | 11 | 19 | 225 |
| pfh | 10 | 14 | 24 | 441 |
| sdgi | 12 | 17 | 29 | 784 |





Matrix of the Hamiltonian for the 126-184 shell

| | $\frac{1}{6}[611]$ |] [600] } | $\frac{3}{5}[602]$ | 1 [631]] | | [613] · | $\frac{1}{5}[620]$ | 3 [611] | 5 [602]] | [604]] | [[651]] | $\frac{3}{642}$ | [(633)] | [624] 8 | [615] | [[640] | 3 [631] - | 5 [622] | 7 [613] - | 8 [604] - | 11 [606] | 1 [770]] | 3 [761] 5 | [752] 3 | [743] { | 2[734] 1 | 1 [725] | 1716] 15 | [707] |
|-----------|--------------------|----------------------|--------------------|-------------------------|------|---------|--------------------|--------------------|-------------------------|--------------------|---------------------------------|-----------------|---------------------------------|--------------------|-------|--------------------|----------------------|------------|----------------------|----------------------|-------------|-------------------------|-------------------------|------------|------------|---------------------|---------|----------|-------|
| 1/2[611] | 8.05 | -0.16 | <u> </u> | 0.25 | Ċ, | 0 | 0.22 | 0 | <u> </u> | - o | 0 | 0 | Ċ, | <u> </u> | 0 | . <u>.</u> | 0 | 0 | 0 | 0 | ů č | 0 | 0 | . <u>.</u> | . <u>.</u> | · | Ó | <u> </u> | - Ó |
| 1/2[600] | | 8.53 | 0 | 0 | 0 | 0 | 0.17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3/2[602] | | | 8.58 | 0 | 0 | 0 | 0 | 0.18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[631] | | | | 7.24 | 0 | 0 | -0.22 | 0 | 0 | 0 | 0.26 | 0 | 0 | 0 | 0 | 0.25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3/2[622] | | | | | 7.61 | 0 | 0 | -0.18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.27 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5/2[613] | | | | | | 8.01 | 0 | 0 | -0.13 | 0 | 0 | 0 | 0.20 | 0 | 0 | 0 | 0 | 0.25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[620] | | | | | | | 7.56 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3/2[611] | | | | | | | | 7.92 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5/2[602] | | | | | | | | | 8.32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7/2[604] | | | | | | | | | | 8.46 | 0 | 0 | 0 | 0.13 | 0 | 0 | 0 | 0 | 0.20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[651] | | | | | | | | | | | 6.77 | 0 | 0 | 0 | 0 | -0.20 | 0 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3/2[042] | | | | | | | | | | | | 0.97 | 7.04 | 0 | | | -0.18 | 0.10 | | | 0 | 0 | 0 | | | | 0 | 0 | 0 |
| 7/2[033] | | | | | | | | | | | | | (.21 | 7.40 | | | | -0.16 | 0.12 | | 0 | | 0 | | | | | 0 | |
| 0/2[024] | | | | | | | | | | | | | | 1.49 | 7.91 | | | | -0.13 | 0.00 | 8 | | | | | | | | |
| 1/2640 | | | | | | | | | | | | | | | 1.01 | 6 92 | ă | ŏ | ŏ | -0.09 | ŏ | ŏ | ő | ŏ | ä | ŏ | ŏ | ő | ŏ |
| 3/2[631] | | | | | | | | | | | | | | | | | 7 12 | ŏ | ŏ | ŏ | ŏ | ŏ | ŏ | ŏ | ŏ | ŏ | ŏ | ŏ | ŏ |
| 5/2[622] | | | | | | | | | | | | | | | | | | 7.35 | ŏ | ő | ŏ | ŏ | ŏ | ŏ | ŏ | ŏ | ŏ | ŏ | ŏ |
| 7/2 613 | | | | | | | | | | | | | | | | | | 1.000 | 7.63 | ŏ | ŏ | õ | ŏ | ŏ | ŏ | ŏ | ŏ | ŏ | ŏ |
| 9/2[604] | | | | | | | | | | | | | | | | | | | | 7.95 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11/2[606] | | | | | | | | | | | | | | | | | | | | | 8.17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[770] | | | | | | | | | | | | | | | | | | | | | | 7.53 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3/2[761] | | | | | | | | | | | | | | | | | | | | | | | 7.52 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5/2[752] | | | | | | | | | | | | | | | | | | | | | | | | 7.55 | 0 | 0 | 0 | 0 | 0 |
| 7/2[743] | | | | | | | | | | | | | | | | | | | | | | | | | 7.62 | 0 | 0 | 0 | 0 |
| 9/2[734] | | | | | | | | | | | | | | | | | | | | | | | | | | 7.74 | 0 | 0 | 0 |
| 11/2[725] | | | | | | | | | | | | | | | | | | | | | | | | | | | 7.89 | 0 | 0 |
| 13/2[716] | | | | | | | | | | | | | | | | | | | | | | | | | | | | 8.089 | 0 |
| 15/2[707] | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 8.32 |

Matrix of the Hamiltonian for the sdgi shell

| | $\frac{1}{2}[611]$ | $\frac{1}{2}[600]$ | $\frac{3}{2}[602]$ | $\frac{1}{2}[631]$ | $\frac{3}{2}[622]$ | 5 [613] | $\frac{1}{2}[620]$ | $\frac{3}{9}[611]$ | $\frac{5}{2}[602]$ | $\frac{7}{2}[604]$ | $\frac{1}{6}[651]$ | 3 [642] · | 5 [633] | $\frac{7}{2}[624]$ | $\frac{9}{2}[615]$ | $\frac{1}{2}[640]$ | $\frac{3}{2}[631]$ | $\frac{5}{2}[622]$ | $\frac{7}{2}[613]$ | 8 [604] | $\frac{11}{2}[606]$ | $\frac{1}{2}[660]$ | 3 [651] | $\frac{5}{2}[642]$ | $\frac{7}{2}[633]$ | $\frac{9}{2}[624] \frac{1}{2}$ | $\frac{1}{2}[615] \frac{1}{2}$ | 3 [606] |
|----------------------|--------------------|--------------------|--------------------|--------------------|--------------------|------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------|------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|------------|---------------------|--------------------|---------|--------------------|--------------------|--------------------------------|--------------------------------|---------|
| 1/2[611] | 8.05 | -0.16 | 0 | 0.25 | 0 | 0 | 0.22 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[600] | | 8.53 | 0 | 0 | 0 | 0 | 0.17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3/2[602] | | | 8.58 | 0 | 0 | 0 | 0 | 0.18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[631] | | | | 7.24 | 0 | 0 | -0.22 | 0 | 0 | 0 | 0.26 | 0 | 0 | 0 | 0 | 0.25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3/2[622] | | | | | 7.61 | 0 | 0 | -0.18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.27 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5/2[613] | | | | | | 8.01 | 0 | 0 | -0.13 | 0 | 0 | 0 | 0.20 | 0 | 0 | 0 | 0 | 0.25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[620] | | | | | | | 7.56 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3/2[611] | | | | | | | | 7.92 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5/2[602] | | | | | | | | | 8.32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7/2[604] | | | | | | | | | | 8.46 | 0 | 0 | 0 | 0.13 | 0 | 0 | 0 | 0 | 0.20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1/2[651] | | | | | | | | | | | 6.77 | 0 | 0 | 0 | 0 | -0.20 | 0 | 0 | 0 | 0 | 0 | 0.22 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3/2[642] | | | | | | | | | | | | 6.97 | 0 | 0 | 0 | 0 | -0.18 | 0 | 0 | 0 | 0 | 0 | 0.28 | 0 | 0 | 0 | 0 | 0 |
| 5/2[633] | | | | | | | | | | | | | 7.21 | 0 | 0 | 0 | 0 | -0.16 | 0 | 0 | 0 | 0 | 0 | 0.31 | 0 | 0 | 0 | 0 |
| 7/2[624] | | | | | | | | | | | | | | 7.49 | 0 | 0 | 0 | 0 | -0.13 | 0 | 0 | 0 | 0 | 0 | 0.31 | 0 | 0 | 0 |
| 9/2[615] | | | | | | | | | | | | | | | 7.81 | 0 | 0 | 0 | 0 | -0.09 | 0 | 0 | 0 | 0 | 0 | 0.28 | 0 | 0 |
| 1/2[640] | | | | | | | | | | | | | | | | 6.92 | 0 | 0 | 0 | 0 | 0 | 0.23 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3/2[631] | | | | | | | | | | | | | | | | | 7.12 | 0 | 0 | 0 | 0 | 0 | 0.26 | 0 | 0 | 0 | 0 | 0 |
| 5/2[622] | | | | | | | | | | | | | | | | | | 7.35 | 7 00 | | 0 | 0 | 0 | 0.25 | 0 00 | 0 | 0 | 0 |
| 7/2[613] | | | | | | | | | | | | | | | | | | | 7.63 | 7.05 | 0 | 0 | 0 | | 0.20 | 0 40 | 0 | 0 |
| 9/2[604] | | | | | | | | | | | | | | | | | | | | 7.95 | 0.47 | 0 | 0 | 0 | 0 | 0.13 | 0 00 | 0 |
| 11/2[606] | | | | | | | | | | | | | | | | | | | | | 8.17 | - 40 | 0 | 0 | 0 | 0 | 0.22 | 0 |
| 1/2[660] | | | | | | | | | | | | | | | | | | | | | | 7.40 | | | 0 | | 0 | 0 |
| 3/2[651] | | | | | | | | | | | | | | | | | | | | | | | 7.44 | | | | 0 | 0 |
| 3/2[042] 7/2[622] | | | | | | | | | | | | | | | | | | | | | | | | 7.01 | ~ e2 | | | |
| 0/2[033] | | | | | | | | | | | | | | | | | | | | | | | | | 7.62 | | 0 | 0 |
| 3/2[024] | | | | | | | | | | | | | | | | | | | | | | | | | | 1.10 | 7.07 | 0 |
| 13/2606 | | | | | | | | | | | | | | | | | | | | | | | | | | | 1.01 | 8.21 |
| 10/2000 | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

• The changes inflicted on the Nilsson diagrams by the replacement of the parity orbitals with their 0[110] counterparts do not change the main features of the diagrams

• This is because the "intruder" parity orbitals have the same orbital angular momentum , spin and total angular momentum

 It is expected that several physical properties of the relevant heavy deformed nuclei can be correctly determined by the new proxy SU(3) scheme

THANK YOU FOR YOUR TIME!!!